

REMARKS

In the Office Action mailed on June 2, 2009, the Examiner restricted the claims of the application and requested that the Applicants confirm their telephonic election of claims 1-3 and 12-14 (Group I). The Examiner also objected to the specification and claims for utilizing the British standard spelling of "aluminium" instead of the U.S. standard spelling "aluminum." Claim 12 was also objected to on the grounds that it is dependent upon claim 4, a claim withdrawn from consideration. The pending, non-withdrawn claims (i.e., claims 1-3 and 12-14) were considered and rejected. Claims 1-3 were rejected under 35 U.S.C. 102(b) as being anticipated by JP 02129333 to Kudo et al. ("Kudo"); claims 1-3 were also rejected under 35 U.S.C. § 102(b) as being anticipated by JP 04202735 to Dokou ("Dokou"); claims 12-13 were rejected under 35 U.S.C. § 102(b) as anticipated by or in the alternative obvious under 35 U.S.C. § 103 in view of Kudo; claims 12-13 were rejected under 35 U.S.C. § 102(b) as anticipated by or in the alternative obvious under 35 U.S.C. § 103 in view of Dukou; claim 14 was rejected under 35 U.S.C. § 103 as obvious in view of Kudo; claim 14 was rejected under 35 U.S.C. § 103 as obvious in view of Dokou; claims 1-3 and 12-14 were rejected under 35 U.S.C. § 103 as obvious in view of EP 0718072 to Miller ("Miller"); and claims 1-3 and 12-14 were rejected under 35 U.S.C. § 103 as obvious in view of U.S. Patent 6,391,129 to Hurd ("Hurd"). As a result, claims 1-3 and 12-14 have been rejected as anticipated by or obvious in view of the disclosures of each of Kudo, Dukou, Miller, and Hurd, independently.

In the attached amendment, Applicants have cancelled claims 1-3 and have withdrawn claims 4-11. Claims 12-14 have been amended to further clarify the invention. Support for amendments to claims 12-14 can be found, for example, on pages 4-5 and 9 of the English Translation as originally filed. No new matter has been introduced by these amendments.

Applicants also amended the specification to: (1) insert the priority information which appears on the filing receipt (2) to correct the spelling of aluminum and (3) to correct clerical and typographical errors as shown on pages 11 and 15 of the enclosed Substitute Specification Marked-Up Version. No new matter has been introduced by this amendment to the specification. Applicants respectfully request that the pending specification be replaced with the enclosed clean Substitute Specification.

In view of the amendments to the claims and specification, together with the following remarks, Applicants respectfully request reconsideration and withdrawal of all grounds of objection and rejection.

Election/Restriction Requirement

Applicants confirm the election of Group I (claims 1-3 and 12-14) as made by attorney, Deborah Vernon, telephonically on May 28, 2009. Applicants also note that after the entry of the attached claim amendment, only claims 12-14 will be considered for examination. That is, claims 1-3 have been cancelled and claims 4-11 have been withdrawn.

Claim Objections

Claims 1-3 and 12-14 were objected to for reciting the British standard spelling “aluminium” instead of the U.S. standard spelling of “aluminum.” In addition, claim 12 was objected to for being dependent upon withdrawn claim 4.

In response, Applicants have cancelled claims 1-3 and have amended claims 12-14 to properly recite “aluminum” rather than “aluminium.” In addition, claim 12 has been further amended to remove reference to claim 4. In view of the amendments made, Applicants request reconsideration and the withdrawal of the objections to the claims.

The Rejection of Claims 1-3 and 12-14 in View of the Disclosures of Each of Kudo, Dukou, Miller, and Hurd, Independently.

The sole, pending independent claim is claim 12. Claim 12 is directed to an aluminum strip or sheet which is comprised of an aluminum alloy having the following proportions of alloy components in weight percent $0.3\% \leq \text{Si} \leq 1\%$, $\text{Fe} \leq 0.5\%$, $0.3\% \text{ Cu} \leq 0.7\%$, $1.1\% \text{ Mn} \leq 1.8\%$, $0.15\% \leq \text{Mg} \leq 0.6\%$, $0.01\% \leq \text{Cr} \leq 0.3\%$, $\text{Zn} \leq 0.10\%$, $\text{Ti} \leq 0.3\%$, unavoidable impurities separately representing a maximum of 0.1%, together a maximum of 0.15%. The aluminum strip or sheet is also defined by its high yield strength. Specifically, the aluminum strip or sheet has a yield strength of greater than 65 MPa not only at room temperature, but also at a temperature of 250 °C. As a result, the claimed aluminum strip or sheet, made from a particular aluminum alloy, has a yield strength of greater than 65 MPa even when heated to 250 °C.

It is believed that the high yield strength of the aluminum strip or sheet of the claim 12 is a result of not only the composition of the aluminum alloy but also its microstructure, which is created by processing. As described on page 9 of the English translation (or paragraph [0025] of the published application), it is the combination of continuous casting of an ingot having the claimed aluminum alloy composition, preheating this ingot to 400 to 500 °C prior to hot rolling, rolling the ingot to a hot strip with a thickness of 3 to 10 mm at a temperature between 250 °C and 380 °C, which leads to a high secondary phase density within the aluminum strip or sheet. It is this high secondary phase density which provides the aluminum strip or sheet with high heat resistance at both room temperature and at a temperature of 250 °C, and thus increases the yield strength of the aluminum strip or sheet to a value greater than 65 MPa at both room temperature and at a temperature of 250 °C. That is, the high secondary phase density in the strip or sheet stabilizes the aluminum alloy, which results in high strength at elevated temperatures.

In order to achieve Applicants' claimed aluminum strip or sheet having a yield strength of greater than 65 MPa at a temperature of 250 °C, an aluminum strip or sheet formed from the claimed aluminum alloy has to be processed to achieve a high secondary phase density. Applicants have discovered that the combination of preheating an ingot of the claimed aluminum alloy to 400 to 500 °C prior to hot rolling and hot rolling the ingot to a hot strip (thickness 3 to 10 mm) at a temperature between 250 °C and 380 °C, creates the high secondary phase density. Conventional temperatures utilized in pre-heating steps prior to hot rolling of an aluminum strip or sheet are higher than 400 to 500 °C. Usually, pre-heating prior to rolling is done at a temperature of about 550 °C in order to reduce rolling forces and to allow for greater recrystallization during hot rolling. Conventional hot rolling temperatures are also at about 550 °C. As a result of utilizing the typical processing (pre-heating and rolling at temperatures of about 550 °C), conventional aluminum strip or sheet does not achieve a high secondary phase density, and thus does not have a yield strength greater than 65 MPa at both room temperature AND at a temperature of 250 °C.

None of the cited references disclose or suggest an aluminum strip or sheet that are formed from an aluminum alloy having the claimed composition and have a yield strength greater than 65 MPa at a temperature of 250 °C. In addition, none of the cited references disclose processing their specific aluminum alloys to achieve a high secondary phase density (which is the source of the high yield strength at 250 °C). Nor do any of the cited references

teach or suggest processing of their alloys, which would lead to a high secondary phase density. That is, none of the cited references teach or suggest preheating an ingot of the claimed composition to 400 to 500 °C prior to hot rolling, rolling the ingot to a hot strip with a thickness of 3 to 10 mm at a temperature between 250 °C and 380 °C. Nor do any of the cited references teach or suggest modifying or straying from conventional processing so as to reduce preheating or hot rolling temperatures. Therefore, Applicants respectfully submit that none of the cited references teach or suggest an aluminum strip or sheet made from an aluminum alloy having the claimed composition and a yield strength of greater than 65 MPa at a temperature of 250 °C.

None of the cited references disclose a yield strength value at 250 °C. As their disclosures also do not teach or suggest the same or similar processing steps to achieve the high secondary phase density required for obtaining a yield strength value of greater than 65 MPa at 250 °C, Applicants submit that the aluminum strip or sheet of claim 12 is neither anticipated or obvious in view of the cited references. For example, Kudo and Dukou neither provide the yield strength at 250 °C nor is there any information provided about processing of the aluminum alloy. (See abstracts and tables of Kudo and Dukou). As a result, a person of ordinary skill in the art would assume that the temperatures used for pre-heating and hot rolling of the aluminum in Kudo and Dukou are greater than 500 °C, which would not result in a high secondary phase density. Thus, neither Kudo nor Dukou teach or suggest an aluminum strip or sheet which has a yield strength of greater than 65 MPa at 250 °C. Miller discloses yield strength values only at room temperature and not at an elevated temperature of 250 °C. In addition, Miller's process for forming the sheet differs from the method used by Applicants to obtain a high secondary phase density (i.e., to obtain a yield strength value greater than 65 MPa at 250 °C). See for example, paragraphs [0028]-[0029] of Miller, which discuss processing but fail to disclose preheating of the alloy at 400 °C to 500 °C or hot rolling to a thickness of 3 to 10 mm at a temperature of between 250 and 380 °C and Table 3 and paragraph [0048] of Miller, which discuss yield strength values taken below 250 °C. Since Miller is completely silent about temperatures during pre-heating and hot rolling, one of ordinary skill in the art would take known parameters into account. These known parameters are deemed to be used in Miller, since, in contrast to the aluminum sheets or strips manufactured by in accordance with Applicants' claim 12, Miller reports about natural and artificial ageing properties resulting in an increasing strength. Miller does not disclose Applicants' reduced age hardening characteristics, which is caused by the

different microstructures present in Applicants' claimed aluminum strips or sheets. See for example, embodiment C4 in table 3 of Miller, which shows an increase of yield strength of 20% after naturally age hardening compared to pages 5 and 6 of Applicants' English Translation, which discusses the reduced age hardening characteristic of the claimed aluminum sheet or strip. As a result, Miller fails to anticipate or suggest Applicants' claimed aluminum strip or sheet having a yield strength value greater than 65 MPa at 250 °C. Hurd also only discloses yield strength values at room temperature and not at an elevated temperature of 250 °C. In addition, Hurd's disclosed process of treatment of the alloy differs from the process Applicants have identified as causing the high secondary phase density, which provides the high value for yield strength at 250 °C. See for example, col. 5, lines 51 to col. 7, line 25, describing a method in which the alloy is preheated to a temperature of 500 to 540 °C and then extruded at a temperature also of between 500 to 540 °C. During extrusion, the aluminum alloy achieves a totally different microstructure, which cannot be compared to the microstructure achieved by hot rolling of an ingot and cold rolling to the final thickness. Extrusion at such temperatures (i.e., 500 to 540 °C) does not create a high secondary phase density. Without the high secondary phase density, the alloy will not be stabilized at elevated temperatures (e.g., such as at 250 °C) and a yield strength of greater than 65 MPa will not be achieved. Accordingly, Hurd too fails to anticipate or make obvious Applicants' aluminum strip or sheet as described in claim 12.

In view of the foregoing, Applicants respectfully request reconsideration and the withdrawal of all objections and rejections to the pending claims, claims 12-14.

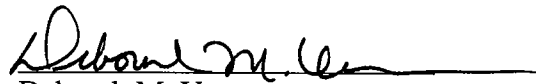
CONCLUSION

Applicants respectfully submit that all of the pending claims are in condition for allowance and requests early favorable action. If the Examiner believes a telephonic interview would expedite the prosecution of the present application, the Examiner is welcome to contact Applicants' Attorney at the number below.

Respectfully submitted,

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HEAT RESISTANT ~~ALUMINIUM~~ ALUMINUM ALLOY FOR HEAT EXCHANGERS

RELATED APPLICATIONS

This application is a National Phase Application of International Application No. PCT/EP2005/03398, filed on March 31, 2005, which claims the benefit of and priority to German patent application no. DE 10 2004 016 482.7, filed on March 31, 2004.

BACKGROUND

The invention relates to a heat resistant ~~aluminium~~ aluminum alloy for heat exchangers, a method for producing an ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet for heat exchangers, and a corresponding ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet.

In the automotive sector there is an increasing tendency to use heat exchangers made of ~~aluminium~~ aluminum or ~~aluminium~~ aluminum alloys. The use of ~~aluminium~~ aluminum instead of the previously customary non-ferrous metal heat exchangers has hereby almost halved the weight of the heat exchangers for comparable size and performance. The heat exchangers made of ~~aluminium~~ aluminum or of an ~~aluminium~~ aluminum alloy are nowadays used in the motor vehicle mostly for cooling the cooling water or the oil, as charge air cooler and in air conditioners. Heat exchangers for motor vehicles are usually produced from ~~aluminium~~ aluminum strips or ~~aluminium~~ aluminum sheets, by joining together the individual prefabricated components of the heat exchanger, such as for example fins, tubes and distributors, by way of brazing. In practical applications, the loads acting on components produced in this way and installed in motor vehicles, are considerable due to shock-like juddering, long-duration vibrations, corrosion, high operating pressures, high operating temperatures and temperature changes. In spite of the considerable loads and increasing operating pressures of the heat exchangers in the motor vehicle, there is still a prevailing trend toward weight savings in the motor vehicle and, with it, toward a further reduction of the wall thickness of the heat exchangers. Moreover, the stricter legislation in the EU and in the USA with respect to the

emission standards leads to additionally increased operating temperatures, for example of charge air coolers, so that the demands on the heat resistance of the ~~aluminium~~ aluminum alloy subsequent to brazing continue to rise. With the ~~aluminium~~ aluminum alloys for heat exchangers used so far, it was only possible to reach values with respect to the strength determining yield strength $R_{p0.2}$ of less than 65 MPa, and of markedly less than 65 MPa at high temperatures of about 250° C, subsequent to brazing. In view of further wall reductions, these values for the yield strength are no longer adequate to meet future demands on heat exchangers. A known means to increase the heat resistance of ~~aluminium~~ aluminum alloys is the alloying into the ~~aluminium~~ aluminum alloy of, for example, the elements Ni, Zr or rare earths in greater or lesser doses. These alloy components are however not usually contained in ~~aluminium~~ aluminum alloys and present damaging effects in application cases other than brazed heat exchangers. In this respect, the alloying of the abovementioned alloy components represents a great problem in regard to the recyclability of the ~~aluminium~~ aluminum alloy, also in view of the EU end-of-life vehicle directive. The methods most frequently used for the production of heat exchangers are, on the one hand, flux-free vacuum brazing and, on the other hand, brazing in a protective gas using non-corrosive fluxes. The age hardening ~~aluminium~~ aluminum alloys used so far for vacuum brazing, for example the ~~aluminium~~ aluminum alloy AA6063 (AlMgO, 7Si), AA6061 (AlMg1SiCu) or AA6951 (AlMgO, 6SiCu), have relatively high magnesium contents and are generally brazed with solders having a high Mg content, such as for example AA4004, in order to, on the one hand, prevent oxidation by gettering of the molten ~~aluminium~~ aluminum solder on the components to be brazed during the vacuum brazing process, thus ensuring a faultless brazed joint without flux, and, on the other hand, achieve high strength values of the brazed heat exchangers for natural ageing subsequent to brazing. In the case of vacuum brazing, it is a disadvantage that the preservation of the vacuum and the purity demands on the components to be brazed are cost-intensive. In view of this, the alternative brazing in a protective gas is less cost-intensive because the brazing takes place in a protective atmosphere comprising an inert protective gas, for example nitrogen. Furthermore, brazing in a protective gas enables up to 20% shorter brazing cycles, but it is not possible to use the ~~aluminium~~ aluminum alloy with high magnesium contents known from vacuum brazing because the magnesium reacts with the non-

corrosive flux during the brazing. The workability can be extended to higher Mg contents by applying expensive caesium containing fluxes. Brazing in a protective gas, also called CAB brazing, is the most important process for producing heat exchangers for the automotive industry. In addition, salt bath brazing is also available, where the components are preheated and subsequently immersed in a salt bath. The salt bath is both flux and transport medium for the heat. The liquid salt reacts with the oxide skin and enables the wetting reaction of the solder, which is protected by the flux. After the holding time at brazing temperature, the heat exchangers are driven out of the salt bath, whereby it must be ensured that the liquid salt is drained. Because the fluxes used for salt bath brazing are normally hygroscopic and contain chlorides, all heat exchangers must be cleaned in a multiple step process subsequent to the salt bath brazing to avoid corrosion problems. In order to prevent a fusion of the core ~~aluminium~~ aluminum alloy of the heat exchanger elements to be brazed in one of the three described brazing methods, the ~~aluminium~~ aluminum alloy should furthermore have a solidus temperature of at least 620° C.

SUMMARY OF THE INVENTION

In view of the above, it is an object of the present invention to provide an ~~aluminium~~ aluminum alloy and an ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet, which has good recyclability, a solidus temperature of at least 620° C and also an improved heat resistance subsequent to brazing. It is a further object of the present invention to provide a method for producing a corresponding ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet.

According to a first teaching of the present invention, the object described above is solved by an ~~aluminium~~ aluminum alloy for heat exchangers, wherein the ~~aluminium~~ aluminum alloy comprises in weight percent:

$$0.3 \% \leq \text{Si} \leq 1 \%,$$

$$\text{Fe} \leq 0.5 \%,$$

$$0.3 \% \leq \text{Cu} \leq 0.7 \%,$$

$1.1 \% \leq \text{Mn} \leq 1.8 \%$,

$0.15 \% \leq \text{Mg} \leq 0.6 \%$,

$0.01 \% \leq \text{Cr} \leq 0.3 \%$,

$\text{Zn} \leq 0.1 \%$,

$\text{Ti} \leq 0.3 \%$,

unavoidable impurities separately representing a maximum of 0.1%, together a maximum of 0.15%, and the remainder being ~~aluminium~~ aluminum.

The ~~aluminium~~ aluminum alloy according to the invention does not only feature a solidus temperature of more than 620° C, but it also has a particularly high heat resistance subsequent to brazing. The ~~aluminium~~ aluminum alloy according to the invention enables the production of heat exchanger elements, for example tubes, the yield strength $R_{p0.2}$ of which is greater than 65 MPa both at room temperature and at a test temperature of 250° C, subsequent to brazing of the heat exchangers. In comparison with the conventional ~~aluminium~~ aluminum alloys, in particular a AA3005 alloy, heat exchanger elements produced from the ~~aluminium~~ aluminum alloy according to the invention thus have a greater than 20% higher heat resistance, in particular also at temperatures of up to 265° C. The attainable heat resistance is ascribed to achieving a high secondary phase density by combining an increased Si, Mn and Cr content with the ~~aluminium~~ aluminum alloy according to the invention. In addition, the ~~aluminium~~ aluminum alloy according to the invention has a greater positive corrosion potential of -750 mV. Elements such as tubes, tube plates, side parts or disks of a heat exchanger produced from the ~~aluminium~~ aluminum alloy according to the invention enable the corrosion design of the heat exchanger to be laid out in such a way that the described elements of the heat exchanger have a high corrosion resistance. Moreover, the ~~aluminium~~ aluminum alloy according to the invention presents merely a reduced age hardening characteristic, so that the ~~aluminium~~ aluminum strips or ~~aluminium~~ aluminum sheets comprising the ~~aluminium~~ aluminum alloy according to the invention are not subjected to storage time limitations prior to processing or forming prior to brazing.

Subsequent to brazing of components of a heat exchanger made from the ~~aluminium~~ aluminum alloy according to the invention, it was further surprisingly found that a good corrosion resistance is achieved in spite of the elevated Cu content.

The proportion in the alloy of the alloy component Si of 0.3 to 1.0 weight percent leads, in combination with the alloy proportions of the remaining alloy components, to the strength of the ~~aluminium~~ aluminum alloy being sufficiently high subsequent to brazing and, at the same time, to the melting point not decreasing. Upon leaving this range of the Si content, when falling below the lower limit of the Si content, the strength of the ~~aluminium~~ aluminum alloy becomes too low subsequent to brazing and, when exceeding the upper limit of the Si content, the solidus temperature is reduced to a value below 620° C. The limitation of the Fe content of the ~~aluminium~~ aluminum alloy according to the invention to a maximum of 0.5 weight percent improves, in conjunction with the Cu content according to the invention, the corrosion resistance of the ~~aluminium~~ aluminum alloy subsequent to brazing. During brazing, the layers in the proximity of the surface of the core material made of the ~~aluminium~~ aluminum alloy according to the invention are depleted from copper, so that a protecting potential gradient to the nobler core material with greater Cu content is generated. This behaviour of the ~~aluminium~~ aluminum alloy during brazing is promoted by the low iron content. The heat resistance of the ~~aluminium~~ aluminum alloy according to the invention drops noticeably at a Cu content of less than 0.3 weight percent; upon exceeding the upper limit of the Cu content, the ~~aluminium~~ aluminum alloy has, however, a tendency to heat cracking during casting. Furthermore, corrosion and brazing problems arise for greater Cu contents as a result of the layers in the proximity of the surface of the core material having a relatively high Cu content, despite depletion. On the one hand, the Mn content of the ~~aluminium~~ aluminum alloy according to the invention determines the size of the segregations. On the other hand, the Mn content has also an influence on the heat resistance. If the amount of manganese in the ~~aluminium~~ aluminum alloy according to the invention falls below the lower limit of 1.1 weight percent, the heat resistance of the ~~aluminium~~ aluminum alloy is reduced. An increase of the manganese content above the upper limit of 1.8 weight percent leads, in contrast, to coarse segregations in the structure, which have a largely negative influence

on the formability of the ~~aluminium~~ aluminum alloy. The strength of the ~~aluminium~~ aluminum alloy subsequent to brazing is additionally influenced by the Mg content. A reduction of the Mg content below 0.15 % leads to poor strength of the ~~aluminium~~ aluminum alloy. The upper limit of the Mg content of 0.6 weight percent ensures that the ~~aluminium~~ aluminum alloy according to the invention is brazeable with all three conventional brazing methods, the vacuum, CAB and salt bath methods. The inventive Cr content of the ~~aluminium~~ aluminum alloy of at least 0.01 weight percent ensures, on the one hand, that the ~~aluminium~~ aluminum alloy according to the invention has sufficient heat resistance. On the other hand, the formability of the ~~aluminium~~ aluminum alloy according to the invention is ensured by limiting the Cr content to a maximum of 0.3 weight percent, since coarse segregations in the crystal structure of the ~~aluminium~~ aluminum alloy are found in the case of said Cr content being exceeded. In order for the ~~aluminium~~ aluminum alloy according to the invention to be ideally suited for producing tube strip, tube plate strip, side part strip and disk strip, the Zn content of the ~~aluminium~~ aluminum alloy is limited to a maximum of 0.1 weight percent. A higher Zn content leads to a reduction of the corrosion potential of the ~~aluminium~~ aluminum alloy, so that the ~~aluminium~~ aluminum alloy is, for example, too ignoble relative to Zn-free fins. Lastly, the inventive Ti content of no more than 0.3 weight percent ensures that no coarse segregations are formed in the ~~aluminium~~ aluminum alloy, which would, in turn, have a negative influence on the formability of the ~~aluminium~~ aluminum alloy.

If the ~~aluminium~~ aluminum alloy according to the invention has, according to another further developed embodiment, the following proportions of alloy components in weight percent:

$$0.15 \% \leq \text{Mg} \leq 0.3 \%$$

$$\text{Zn} \leq 0.05 \%$$

$$0.01 \% \leq \text{Ti} \leq 0.3 \%,$$

the ~~aluminium~~ aluminum alloy according to the invention can be processed according to the CAB brazing method without expensive caesium containing fluxes, with the risk of cracks

during solidification of the rolling ingot simultaneously being reduced by the Ti content and the corrosion potential being increased by the reduced Zn content.

A very good compromise of maximum strength subsequent to brazing and simultaneously high solidus temperature is achieved, according to a further embodiment of the ~~aluminium~~ aluminum alloy according to the invention, by the ~~aluminium~~ aluminum alloy comprising the following proportions of the alloy components Si, Fe and Mn in weight percent:

$$0.5 \% \leq \text{Si} \leq 0.8 \%,$$

$$\text{Fe} \leq 0.35 \%,$$

$$1.1 \% \leq \text{Mn} \leq 1.5 \, \%.$$

According to a second teaching of the invention, the object described above is solved by a method for producing an ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet for heat exchangers, wherein a rolling ingot made of a heat resistant ~~aluminium~~ aluminum alloy according to the invention is cast in a continuous casting process, the rolling ingot is preheated at 400 to 500° C prior to hot rolling, the rolling ingot is rolled to a hot strip, with the hot strip temperature being 250 to 380° C, the hot strip is rolled to a hot strip thickness of 3 to 10 mm at the end of the hot rolling and the hot strip is cold rolled to final thickness. An ~~aluminium~~ aluminum strip having a high secondary phase density can be produced by combining the described method features for producing an ~~aluminium~~ aluminum strip, in conjunction with the ~~aluminium~~ aluminum alloy according to the invention. As a result of the high secondary phase density, an ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet according to the invention has a high thermal resistance at room temperature and at a temperature of 250° C. The yield strength Rp0.2 of the ~~aluminium~~ aluminum strip is greater than 65 MPa at the above mentioned temperatures.

If the ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet is to be a side part strip, disk strip or tube plate strip, then, according to another further developed embodiment of the

invention, the ingot can be homogenized prior to preheating. As a result of the deformations which are necessary for producing a tube plate, side part or a disk of a heat exchanger, the ~~aluminium~~ aluminum strip should have a maximum formability prior to the processing to one of the last mentioned elements of a heat exchanger. This is ensured by the homogenization prior to the preheating of the rolling ingot. Unless the ~~aluminium~~ aluminum strip according to the invention does not have to be subjected to severe deformations prior to brazing, such as, for example, for the production of tubes, a homogenization step prior to the preheating can be dispensed with. Although the yield strength $R_{p0.2}$ of the ~~aluminium~~ aluminum strip is reduced by the homogenization prior to the preheating, the yield strength $R_{p0.2}$ is still greater than 50 MPa, in particular also for test temperatures of 250° C, so that yield strengths are achieved, which are far greater than those of the standard alloy AA 3003.

The formability of the ~~aluminium~~ aluminum strip can be further improved by intermediate annealing of the hot strip at a temperature of 300 to 450° C. Alternatively or cumulative thereto, it is possible to subject the ~~aluminium~~ aluminum strip to intermediate annealing at a temperature of 300 to 450° C during cold rolling, prior to achieving the final thickness. By means of the intermediate annealing steps, solidifications, which have been created in the ~~aluminium~~ aluminum strip as a result of deformations, are removed again to a large extent. The process steps mentioned above ensure a maximum formability during cold rolling of the ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet.

The final state of the ~~aluminium~~ aluminum strip is obtained, according to a further developed embodiment of the method according to the invention, by carrying out, subsequent to the cold rolling, a phase annealing step to the final state at a temperature of 250 to 400° C. If the ~~aluminium~~ aluminum strip is used for the production of tube plates, side parts or disks of a heat exchanger, a soft annealing step takes place subsequent to the cold rolling. If tubes are produced from the ~~aluminium~~ aluminum strip, which does not require strong deformations, the ~~aluminium~~ aluminum strip is merely re-annealed subsequent to the cold rolling.

According to another further developed embodiment of the method according to the invention, subsequent to the preheating, the rolling ingot is provided on one or two sides with plates made of another alloy. In this way, the properties of the plate-clad side of the core ingot can be adjusted almost independently from the ~~aluminium~~ aluminum core alloy. The process reliability during brazing of the heat exchanger elements can be increased, for example, by cladding using an ~~aluminium~~ aluminum solder. In addition, other plates comprising non-solder alloys can also be attached to the ~~aluminium~~ aluminum core ingot, for example corrosion protective claddings. When using a plate of ~~aluminium~~ aluminum solder, the ~~aluminium~~ aluminum solder layer is cold-welded to the core ingot during hot rolling, so that the ~~aluminium~~ aluminum strip comprises a uniform cladding layer. This leads to particularly homogenous and uniform brazed joints between the individual elements of the heat exchanger during brazing. In the case of one-sided cladding with an ~~aluminium~~ aluminum solder, it is furthermore possible to clad or to coat the other side with another ~~aluminium~~ aluminum alloy, for example with an ~~aluminium~~ aluminum alloy serving as corrosion protection. ~~Aluminium~~ Aluminum tubes for heat exchangers are clad on one or two sides, depending on requirements. The ~~aluminium~~ aluminum strip for side parts are, however, usually clad on one side. Tube plates and disks of a heat exchanger are, in contrast, used mostly with double-sided cladding.

It is also conceivable to use other alternative solder application methods in conjunction with the ~~aluminium~~ aluminum strip according to the invention.

According to a further embodiment of the method according to the invention, the method according to the invention for producing an ~~aluminium~~ aluminum strip can be improved by using as ~~aluminium~~ aluminum solder an ~~aluminium~~ aluminum alloy comprising 6 to 13 % Si, in particular an AlSi7.5 alloy or AlSi10 alloy. As a result of the high Si content of the solder, the silicon diffuses out of the solder into the core of the ~~aluminium~~ aluminum strip, where it leads to the formation of a segregation seam of AlMnSi phases, which, compared to the core alloy, have a negative corrosion potential. In the case of a corrosion attack on an ~~aluminium~~ aluminum strip produced in accordance with the method according to the invention, the corrosion therefore

develops along the length of the ~~aluminium~~ aluminum strip and along the segregation seam, respectively. The core of the ~~aluminium~~ aluminum strip remains corrosion free and a perforation, for example of a tube produced from a corresponding ~~aluminium~~ aluminum alloy, can thus be prevented. The described ~~aluminium~~ aluminum alloy comprising 6 to 13 weight percent Si, which are used as ~~aluminium~~ aluminum solder, can also contain further elements besides Si, for example 0.5 to 2 weight percent Zn.

By cold rolling the ~~aluminium~~ aluminum strip to a final thickness of 0.1 to 2 mm during cold rolling, heat exchangers having reduced wall thickness can be produced, which nevertheless comply with the stricter future operating requirements.

Moreover, according to a third teaching of the present invention, the object described above is solved by an ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet made of an ~~aluminium~~ aluminum alloy according to the invention, wherein the ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet is produced in accordance with the method according to the invention.

The ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet is preferably a tube strip, a tube plate strip, a side part strip or a disk for producing a heat exchanger. With the tube strip, tube plate strip, side part strip or disk strip according to the invention, corresponding elements of the heat exchanger, tubes, tube plates, side parts or diskis can be produced, which, despite the reduced wall thickness, comply with all the remaining requirements, in particular with regards to the formability prior to brazing and the yield strength at room and operating temperature.

According to an advantageous embodiment of the ~~aluminium~~ aluminum strip according to the invention, the weight of the heat exchangers can be reduced by the tube strip having a final thickness of 0.15 to 0.6 mm, preferably 0.15 to 0.4 mm, the tube plate strip having a final thickness of 0.8 to 2.5 mm, preferably 0.8 to 1.5 mm, the side part strip having a final thickness of 0.8 to 1.8 mm, preferably 0.8 to 1.2 mm or the disk strip having a final thickness of 0.3 to 1.0 mm, preferably 0.3 to 0.5 mm.

There are now a multiplicity of options for further developing and configuring the ~~aluminium~~ aluminum alloy according to the invention, the method according to the invention for producing an ~~aluminium~~ aluminum strip for heat exchangers, and the ~~aluminium~~ aluminum strip. Reference is hereto made, on the one hand, to the patent claims ~~subordinate to the independent patent claims 1, 4 and 12~~ and to the description of exemplary embodiments in conjunction with the drawing, in which

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic representation of a first exemplary embodiment of the method according to the invention for producing an ~~aluminium~~ aluminum strip and

Fig. 2 is a perspective view of a heat exchanger for motor vehicles.

DETAILED DESCRIPTION OF THE DRAWINGS

Fig. 1 shows schematically a first exemplary embodiment of a method according to the invention for producing an ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet for heat exchangers according to the second teaching of the present invention. In a first step, Fig. 1 shows the ingot casting 1. Subsequent to the alloying of the liquid metal, both the ~~aluminium~~ aluminum alloy for the core and the alloy for cladding, for example an ~~aluminium~~ aluminum solder, are cast as ingots. The cladding ingot is usually preheated, hot rolled to the desired thickness and divided longitudinally to produce a plate. The plate can, however, also be produced by using alternative methods, for example by separation from a rolling ingot. The core ingot made of an ~~aluminium~~ aluminum alloy according to the invention can optionally be homogenized from the rolling product to be produced prior to preheating. If, for example, a tube strip for heat exchangers is produced using the method according to the invention, a homogenization step prior to the hot rolling may, however, also be dispensed with, since the tube strip is not subjected to large

deformations prior to production of a tube for heat exchangers. The plates required for cladding are laid on one or both sides of the core ingot. The resulting stack comprising a core ingot, consisting of an ~~aluminium~~ aluminum alloy according to the invention, which is provided with plates on one or two sides, is preheated at 400 to 500° C prior to hot rolling. The stack 4 is then hot rolled in a reversing stand 5 or, alternatively, on a tandem stand 5a to a hot strip thickness of 3 to 10 mm. The hot strip temperature during hot rolling is of 250 to 380° C.

Subsequent to the hot rolling, the strip is cold rolled on a cold roller 6. According to the invention, the strip can be intermediately annealed at a temperature of 300° C to 450° C subsequent to the hot rolling, for example in order to achieve the forming properties. This applies also for the cold rolling, wherein the intermediate annealing can also take place at a temperature of 300° C to 450° C prior to reaching the final thickness. The finished cold rolled ~~aluminium~~ aluminum strip or ~~aluminium~~ aluminum sheet according to the invention can be subjected to a phase annealing step in a batch furnace 7, depending on the properties required. A phase annealing step may, however, also take place in a continuous furnace.

Fig. 2 shows a heat exchanger 8 of a tube/fin design in a perspective view. It can be seen that the heat exchanger is comprised of a tube 9, a tube plate 10, side parts 11 and fins 12. The side parts 11 and the tube plate 10 are subjected to severe deformations prior to brazing, so that the ~~aluminium~~ aluminum strip intended for the side parts 11 and the tube plate 10 should have correspondingly good forming properties. The tubes 10 of the heat exchanger are generally produced by longitudinal seam welding. The thickness of the tube strip processed in this way is of between 0.15 mm and 0.6 mm, preferably 0.15 to 0.4 mm, with the tube strip being solder clad externally or on both sides, depending on the construction type of the heat exchanger. The requirements on the formability of a tube strip are rather low, since it is only subjected to simple forming prior to brazing. Subsequent to brazing, both the resistance and the heat resistance of the tube are very important, since operating media passed through the tubes are subjected to high operating pressures and the tube is partly subjected to high operating temperatures. An ~~aluminium~~ aluminum strip according to the invention for the tube plate 10 typically has a

thickness of 0.8 to 2.5 mm, preferably 0.8 to 1.5 mm, and is preferably produced and processed in the state "soft". For this, subsequent to the cold rolling, the ~~aluminium~~ aluminum alloy according to the invention is annealed to the final state "soft". The requirements on the formability prior to brazing are high for the tube plate strip, since forming is carried out at a high strain rate, which is used for the sealing and fastening of, for example, a water box, a collector, an air connection or similar components. The tube plate strip is normally clad on one side, it can, however, also be clad on both sides. For reasons of corrosion protection, the tube plate 10 and also the tube 9 can comprise another ~~aluminium~~ aluminum alloy as protective cladding, in order to be even more corrosion resistant. The side parts 11 are produced and processed, preferably in the state "soft", from an ~~aluminium~~ aluminum strip comprising an ~~aluminium~~ aluminum alloy according to the invention having a wall thickness of 0.8 to 1.8 mm, preferably 0.8 to 1.2 mm. As for the tube plate 10, the requirements on the formability of the side parts are high. This also applies to a disk of a heat exchanger not shown on Fig. 2, which is used for heat exchangers of the disk-fin type or heat exchangers of the stacked disk type.

Apart from high strength values of the ~~aluminium~~ aluminum alloy, a high corrosion resistance is especially required. With an ~~aluminium~~ aluminum alloy according to the invention, the reduced iron content and increased copper content make an "in-situ formation" of a cathodic corrosion protection possible during the brazing process. Firstly, copper diffuses during brazing from the regions of the core material in the proximity of the cladding layer to the ~~aluminium~~ aluminum solder layer, so that a protective potential gradient to the nobler core material is generated. In addition, silicon diffuses from the ~~aluminium~~ aluminum solder having a high silicon content into the core material of the ~~aluminium~~ aluminum strip according to the invention, where it leads to the formation of a segregation seam comprised of AlMnSi phases. However, compared with the core alloy, the AlMnSi phases have a greater negative corrosion potential. In the case of a corrosion attack on a brazed tube which is produced from an ~~aluminium~~ aluminum strip according to the invention, as a result of the segregation seam, the corrosion will initially continue to develop along the length of the tube and not penetrate the core material, thus being able to prevent a perforation of the tube.

Finally, according to a second exemplary embodiment of the present invention, an ~~aluminium~~ aluminum strip for the production of tubes for heat exchangers was produced according to the method according to the invention and its heat resistance measured. The ~~aluminium~~ aluminum alloy of the ~~aluminium~~ aluminum strip produced had thereby the following alloy composition:

Si = 0.6 wt %,

Fe = 0.3 wt %,

Cu = 0.4 wt %,

Mn = 1.3 wt %,

Mg = 0.3 wt %,

Cr = 0.1 wt %,

Zn = 0.01 wt %,

Ti = 0.02 wt %,

unavoidable impurities separately representing a maximum of 0.1 %, together a maximum of 0.15%, and the remainder being ~~aluminium~~ aluminum.

Subsequent to brazing, the heat resistance was determined by measuring the yield strength. The yield strength Rp0.2 was 72 MPa at a test temperature of 250 °C. Conventional ~~aluminium~~ aluminum alloys have markedly lower yield strengths, in particular at test temperatures of 250° C. The yield strengths of the ~~aluminium~~ aluminum alloys typically used for tubes of a heat exchanger are below 65 MPa at room temperature. For example, subsequent to brazing at a temperature of 250° C, a conventional alloy AA3003 has only a yield strength Rp0.2 of less than 40 MPa. As a result of the gain in heat resistance, with the ~~aluminium~~ aluminum alloy according to the invention and the ~~aluminium~~ aluminum strip according to the invention it is possible to further reduce the wall thicknesses of the tubes, tube plate, side parts and disks of a heat exchanger, without endangering the operating safety of the heat exchangers.

ABSTRACT

The invention relates to a heat-resistant ~~aluminium~~ aluminum alloy for heat exchangers, a method for producing an ~~aluminium~~ aluminum strip or sheet for heat exchangers, and a corresponding ~~aluminium~~ aluminum strip or sheet. The aim of the invention is to provide an ~~aluminium~~ aluminum alloy and an ~~aluminium~~ aluminum strip or sheet which has a good recycling capacity, a Solidus temperature of at least 620° C., and an improved heat-resistance after welding. To this end, the inventive ~~aluminium~~ aluminum alloy comprises the following parts of alloy constituents in ~~wL~~ weight %: $0.3\% \leq \text{Si} \leq 1\%$, $\text{Fe} \leq 0.5\%$, $0.3\% \leq \text{Cu} \leq 0.7\%$, $1.1\% \leq \text{Mn} \leq 1.8\%$, $0.15\% \leq \text{Mg} \leq 0.6\%$, $0.01\% \leq \text{Cr} \leq 0.3\%$, $\text{Zn} \leq 0.10\%$, $\text{Ti} \leq 0.3\%$, unavoidable impurities separately representing a maximum of 0.1%, and together a maximum of 0.15%, the remainder being ~~aluminium~~ aluminum.